Optimal Materials for Maximum Large-Area Near-Field Radiative Heat Transfer

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ABSTRACT: We consider the space of all causal bulk materials, 2D materials, and metamaterials for maximum near-field radiative heat transfer (RHT) between planar structures. Causality constrains the bandwidth over which plasmonic response can occur, explaining two key traits in ideal materials: small background permittivities (minimal high-energy transitions in 2D materials) and Drude-like free-carrier response, which together optimally yield 10× enhancements beyond the theoretical state-of-the-art. We identify transparent conducting oxides, III-nitrides, and graphene as materials that should offer nearly ideal near-field RHT rates, if doped to exhibit plasmonic resonances at what we term “near-field Wien frequencies”. Deep-subwavelength patterning can provide marginal further gains at the expense of extremely small feature sizes. Optimal materials have moderate loss rates and plasmonic response at 19 μm for 300 K temperature, suggesting a new opportunity for plasmonics at mid- to far-infrared wavelengths, with low carrier concentrations and no requirement to minimize loss.

KEYWORDS: near-field radiative heat transfer, 2D materials, Wien’s law, fundamental limits, causality, Kramers–Kronig relations

In this Article, we identify optimal materials and metamaterials for maximum near-field radiative heat transfer (RHT) between large-area planar bodies. We optimize over the space of all causality-allowed material-permittivity or conductivity distributions and discover the possibility for heat-transfer coefficients at the level of 2 × 10^7 W/(m²K) at 10 nm separations (and 300 K temperature), more than 10× higher than the current theoretical state-of-the-art. These bounds enable identification of three key characteristics of optimal materials: small background permittivities (or, for 2D materials, minimal high-energy electronic transitions), moderate loss rates, and a single-pole Drude-like response with ≈19 μm effective surface-plasmon wavelength. These three criteria are not all satisfied by any of the typical bulk materials proposed for near-field RHT; for example, doped silicon has a large background permittivity, while polar dielectrics have a non-Drude-like, highly dispersive narrow-band response. Among bulk materials, we identify transparent conducting oxides (TCOs) and III-nitrides at low to medium carrier concentrations (≈10^18 cm⁻³) as particularly promising material classes, with the capability to exhibit record RHT rates and to approach within a factor of 2 of the causality-based bounds. Among metamaterials, we show that hyperbolic effective-medium response is nonideal and that, although patterned-cylindrical-hole structures can enable slight enhancements to RHT response, they may require unrealistic feature sizes to do so. We use a gap-surface-mode analysis to provide physical intuition supporting the ideal material characteristics, and we derive a “near-field Wien’s Law” to prescribe the optimal resonance frequencies at any temperature.

Because near-field local densities of states cannot scale with the square of frequency, ~ω^2, like far-field plane-wave states do, the optimal near-field resonance frequencies are significantly red-shifted relative to the classical Wien frequencies, yielding optimal HTC rates of (760 W/m² K²)T as a function of temperature T. Interestingly, the optimal causal 2D materials can have slightly superior HTCs to their bulk counterparts, and realistic 2D plasmonic materials at low carrier concentrations or Fermi levels and moderate loss rates also offer the prospect for record-level near-field RHT rates. From a materials perspective, these results offer a new opportunity for plasmonics: instead of pushing for near-zero loss and the highest possible carrier concentrations to exhibit near-visible-frequency resonances, optimal materials have moderate loss rates and support mid- to far-infrared resonances arising from low to moderate carrier concentrations. More broadly, these optimal characteristics we present can provide guidelines for material choices and designs for a wide range of thermal applications in the near field, such as thermophotovoltaics, heat-assisted magnetic recording, nanolithography, and thermal management.

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In recent years, near-field RHT rates significantly higher than the blackbody limit have been measured between SiO\(_2\), SiC, gold, and doped Si in pioneering experiments,\(^1\)\(^{10,21–26}\) inspiring a search for the best material and structure combinations for near-field RHT.\(^{27–33}\) Out of practical materials, polar dielectrics seem sensible for their strong surface phonon polaritonic resonances in the infrared. SiO\(_2\) plates, in particular, could in theory yield 300 K HTC of about 2 \times 10^4 \text{W/(m}^2\text{K)} at 10 nm separations.\(^1\) Plasmonic materials and doped semiconductors, whose strong surface resonances play a large role in near-field RHT, have also been explored.\(^{33,2–24,34}\) Advanced material growth and nanofabrication techniques have enabled wavelength- to deep-subwavelength-scale patterning of materials.\(^{22,35}\) Both hyperbolic metamaterials and in-plane structured metamaterials have been theoretically shown to offer RHT values larger than those of some bulk materials.\(^4\)\(^{5,30,36–37}\) Rigorous-coupled-wave-analysis computations have shown that, at 300 K, air-hole patterned doped Si at a carrier concentration of \(n \approx 10^{20} \text{cm}^{-3}\) can offer a comparable HTC value to that from SiO\(_2\) at 10 nm and even better relative values for larger separations up to 1000 nm.\(^\)\(^\)

A fundamental question yet to be answered is which material properties enable maximal HTC between planar structures at any given temperature. Specific instances of this question have been explored theoretically and computationally.\(^5\)\(^{37–40}\) References \(^38\) and \(^41\) provide modal analyses of gap surface waves, though without intuition about integrated broadband radiative response and optimal material properties. Numerical optimizations for single-pole permittivity lineshapes of materials have been done,\(^39\)\(^40\) but without contextualization in the broader landscape of material possibilities and without guidance relating the optimal single-pole parameters to temperatures, gap distances, and related system parameters. Moreover, none of these works consider optimality criteria of 2D materials. More recent work on analytical bounds and large-scale optimization for near-field RHT\(^32\) have shown that there may be little benefit to improving near-field RHT between extended objects via structuring and that, for a given material, planar structures may be nearly globally optimal. These results suggest that uncovering the optimal material may be the key lever for significant enhancements of near-field RHT. These works help us better delineate our questions: what is the best material for near-field RHT out of all causality-allowed materials, including multiple-pole bulk materials and 2D materials? Can we theoretically explain the optimal parameters? How do the optimal parameters vary with temperature?

We start by doing numerical optimizations in search of the optimal linear permittivity for bulk materials and 2D conductivity for 2D materials at 300 K, with passivity as the only constraint. The results provide not only the largest possible HTC, but also intuitions of optimal material characteristics, which for both bulk and 2D materials, entails that small-background-permittivity single-Drude-pole plasmonic materials with moderate loss could provide the ideal lineshape and that the ideal frequency of peak spectral contribution is about 0.067 eV. Through gap surface resonance modal analyses and rigorous computations of HTC, the temperature-independent optimal material properties can be intuitively explained. As for the optimal resonance frequency (frequency of peak spectral contribution in the case of 2D materials), which varies with the operating temperature, we apply an analysis similar to that leading to Wien’s Law for blackbodies and derive near-field versions that account for the spectral profiles of LDOS. These near-field laws define the optimal resonance frequencies as a function of temperature for bulk materials, with a linear scaling factor significantly smaller than that of a blackbody. Optimal HTC also scales linearly with temperature, different from the cubic dependence in the far-field case. Furthermore, we study the effects of deep-subwavelength patterning under the framework of effective medium theory (EMT) and suggest the optimal schemes and parameters for nanostructuring. Large reductions in carrier concentrations can be provided by in-plane patterning of cylindrical air-holes, yielding enhancement in HTC for originally suboptimal materials. However, originally optimal materials still provide good, if not better, HTC values without nanopatterning, in which sense deep-subwavelength patterning only makes sense if one had to begin with highly suboptimal materials and feature sizes well below the gap distance can be fabricated. Our optimizations over bulk materials and metamaterials effectively encompass thin films as well: at thicknesses larger than the skin depth, they show bulk-like response, and at thicknesses smaller than the skin depth, they show nearly identical response to multilayer hyperbolic metamaterials.\(^42\) Similar optimizations over all causality-consistent 2D conductivity for 2D materials present findings that are excitingly similar to those of bulk materials and can be explained likewise. Despite quite different gap surface resonance modal dispersions for bulk and 2D materials in the plane-plane configuration, the optimal 2D material is the direct 2D analog of the optimal bulk material, as it has a single Drude pole, a moderate loss rate, and minimal higher-energy electronic transitions. Among common materials, we predict that TCOs, III-nitrvides with small background permittivities, bulk or 2D, as well as other 2D-doped semiconductors and 2D semimetals with predominantly single-Drude-pole 2D conductivity, once synthesized and engineered to possess low to medium carrier concentrations and moderate loss levels, could potentially approach the optimal permittivity or the optimal 2D conductivity and yield HTC \(5\times\) better than SiO\(_2\) for a wide range of gap separations.

### IDEAL CAUSALITY-ALLOWED \(\epsilon(\omega)\) FOR MAXIMUM HTC

In this section, we formulate the optimization of heat-transfer coefficients (HTCs) over all causality-allowed material permittivities \(\epsilon(\omega)\). We start with the standard expressions for computing HTC via modal-photon-exchange functions and list common Drude and Drude—Lorentz permittivity lineshapes. In what follows, we describe the Kramers—Kronig-based representation of all causality-consistent permittivities, and we show that numerical optimizations identify key material characteristics that are optimal for near-field RHT. We concentrate on HTC in this section to isolate the effects of a single temperature, which makes it useful for comparisons across the literature, and as discussed in a later section, our results translate seamlessly to RHT between two bodies with arbitrary temperature differences.

### HTC BETWEEN PLANAR STRUCTURES

The canonical configuration of extended near-field RHT consists of two parallel half-spaces (or two parallel planar structures for 2D materials) separated by a vacuum gap with thickness \(d\) much smaller than the characteristic thermally excited wavelength.\(^5\)\(^{16,43}\) For materials with translation and rotation symmetry in the plane parallel to the surfaces (isotropic...
or anisotropic out of plane), HTC is calculated with a double-integration over all plane-wave channels at frequency $\omega$ and surface-parallel wavenumber $\beta$. The infinitesimal frequency difference between the two bodies manifests in a temperature derivative of the Planck distribution $\Theta(\omega, T)$, where $\Theta(\omega, T) = h\omega/(e^{h\omega/k_BT} - 1)$ and $k_B$ is the Boltzmann constant. Then the HTC is given by

$$\text{HTC} = \frac{1}{4\pi^2} \int_0^\infty \frac{d\Theta(\omega, T)}{dT} \int_0^\infty \frac{\xi(\omega, \beta) \delta\beta d\omega}{\Theta(\omega, \beta)}$$

for any polarization. The modal photon exchange rate $\xi(\omega, \beta)$ is proportional to the transmission probability through each plane-wave channel; for evanescent waves, it is given by

$$\xi(\omega, \beta) = \frac{4\text{Im} \varepsilon_0 \text{Im} \varepsilon_{2d} \beta^{2i} e^{2i_k \beta_{i}}}{1 - \varepsilon_0 \varepsilon_{2d} \beta^{2i} e^{2i_k \beta_{i}}}$$

(2)

The contributions from propagating waves are not included in our calculations of near-field RHT throughout, as they are negligible for the highly subwavelength gap separations of interest. Moreover, this allows us to isolate the relevant near-field physics. For isotropic bulk materials, the reflection coefficients $r_{0,i}$ from vacuum gap to medium $i = 1, 2$ are determined by the permittivity $\varepsilon(\omega)$ and the $z$-components of the wavevector in vacuum, $k_{0,z}$ and that in the material, $k_{i,z}$, given by

$$r_{0,i} = \frac{k_{0,z} \varepsilon_i - k_{z}}{k_{0,z} \varepsilon_i + k_{z}}$$

(3)

for TM polarization, which is the dominant near-field channel (the TE-polarized reflection coefficient is given by a similar expression). Hence the $\varepsilon(\omega)$ enters the HTC calculation of eq 1 from the reflectivity of eq 3, mediated by the quantity $\Theta(\omega, \beta)$ that we refer to as the “spectral photon exchange”.

### COMMON PERMITTIVITY LINESHAPES

Metals, doped semiconductors, and polar dielectrics are all materials of interest for large near-field RHT. Their permittivity lineshapes arise from electronic transitions (intraband and interband), optical phonons, and related processes determining optical properties for most materials.

The simplest Drude lineshape can often describe intraband transitions and is given by

$$\varepsilon(\omega) = \varepsilon_{\infty} \left(1 - \frac{\omega_p^2}{\omega^2 + i\gamma}\right)$$

(4)

The background permittivity $\varepsilon_{\infty}$ arises from electronic transitions with frequencies much higher than thermally interesting ones. (Whether it multiplies the second term or not amounts to a simple redefinition of the parameter $\omega_p$.) The plasma frequency, $\omega_p$, the amplitude or strength of the oscillator, is a measure of free-carrier density $n$ (generalized to incorporate background permittivity and effective mass):

$$\omega_p^2 = \frac{ne^2}{\varepsilon_0 m_{\text{eff}}}$$

(5)

where $m_{\text{eff}}$ is the free-carrier effective mass. From electron scattering rate $\gamma$, one can define a dimensionless loss rate $g = \gamma/\omega_p$.

A Drude–Lorentz lineshape, which describes, for example, interband transitions and optical-phonon contributions, is given by

$$\varepsilon(\omega) = \varepsilon_{\infty} \left(1 - \frac{\omega_p^2}{\omega^2 - \omega_0^2 + i\omega\gamma}\right)$$

(6)

where the frequency $\omega_0$ is the band-to-band transition frequency (or reverse-optical-phonon frequency), and the oscillator strength is now denoted by $\omega_p$. Knowledge of the ratio of the static dielectric constant $\varepsilon$ to $\varepsilon_{\infty}$ specifies the ratio $\omega_0^2/\omega_p^2$, which follows from eq 6 and is known as the Lyddane–Sachs–Teller relation.

### NUMERICAL OPTIMIZATION OF $\varepsilon(\omega)$ FOR HTC AT 300 K

Any causal physical material permittivity must satisfy the Kramers–Kronig relations that relate the real part $\Re \varepsilon$ at one frequency $\omega$ to an integral of the imaginary part $\Im \varepsilon$ (or vice versa) over all frequencies ($\omega'$):

$$\Re \varepsilon(\omega) = 1 + \frac{2}{\pi} \int_0^\infty \omega' \Im \varepsilon(\omega') (\omega')^2 - \omega^2 \ d\omega'$$

(7)

where the integral is a principal-value integral. Notice the suggestive form of the integrand of eq 7, which is similar to a lossless Drude–Lorentz oscillator with an integration variable $\omega'$ as the effective transition frequency of a continuum of oscillators. As we show in the SM, this correspondence can be formalized: for a discretization of the Kramers–Kronig relation into local basis functions, one can write the permittivity as a sum of Drude–Lorentz oscillators with infinitesimal loss rates:

$$\varepsilon(\omega) = 1 - \sum_{i=1}^N \frac{\omega_{i}^2}{\omega^2 - \omega_{i}^2 + i\omega\gamma_i}$$

(8)

where $\gamma_i \rightarrow 0$ from above. For anisotropic materials, one could write eq 8 for each of the components of the permittivity tensor, with possible further constraints, and optimize over the resulting permittivity the same way we describe here for scalar permittivity. Anisotropy from two types of metamaterial patterning is studied in the section “Deep-Subwavelength, Possibly Anisotropic, Structured Metamaterials”, where we find that the best anisotropic metamaterial cannot outperform the optimal isotropic material, suggesting that anisotropy is of limited value. For scalar permittivity, such a representation is completely general and applies for arbitrarily high loss levels in a material. (Lossless Drude–Lorentz oscillators have $\delta$-function imaginary parts with arbitrarily large amplitudes, which can be derived from eq 8 in the $\gamma_i \rightarrow 0$ limit, cf. SM.) A similar representation can be derived via a Mittag–Leffler expansion, albeit with possibly lossy oscillators and without consideration of higher-order poles. In some scenarios, one may use alternative oscillator types (e.g., Gauss–Lorentz) which, for a small number of oscillators, may be a better approximation of certain dielectric functions. But ultimately any such permittivity must be representable by eq 8.

Optimizing HTC over all causality-allowed permittivities can then be done by optimizing eq 1 over all possible oscillator strengths $\omega_{i}$ and frequencies $\omega_{0,i}$ (with infinitesimal loss rates $\gamma_i$) for the two materials involved. For a single material, we optimize over these parameters by choosing a large number (hundreds) of oscillator frequencies $\omega_{0,i}$ to cover the full relevant bandwidth. HTC is not a convex function of the parameters, and
parameters starting from a random initial guess, and then using optimizations in two stages: to avoid poor-quality local optima, we typically run the other, and similar conclusion is also obtained in ref 40. To maximize photon tunneling probabilities from one body to the other, and similar conclusion is also obtained in ref 40. The resultant lineshape is predominantly that of a single-pole Drude permittivity with $\omega_{a,0} = 0.094$ eV. (c) Spectral HTC from the initial (blue) and optimal (red) permittivities. Inset: zoomed-in profile of the optimal Re $\epsilon(\omega)$ near the near-field thermal frequency at 300 K, which is derived in the section "Wien Frequencies for Near-Field Energy Exchange between Real Materials".

Figure 1. Numerical optimizations of permittivity profiles to maximize the HTC of the plane–plane configuration at 300 K. (a) Schematic of the plane–plane configuration with bulk materials represented by $\epsilon(\omega)$ and 2D materials by $\sigma(\omega) = \epsilon_0 \omega_\text{R} / (\omega^2 + \omega_\text{R}^2)$. (b) The initial guess (blue) and optimal permittivity profile (red) of one representative 400-oscillator optimization, with a gray dashed line indicating $\epsilon = -1$. Inset shows the corresponding oscillator amplitudes $\omega_{a,i}$. From a random starting point, where all $\omega_{a,i} \neq 0$, the optimization result has the largest nonzero amplitude for the Drude oscillator and only a few small amplitudes for Drude–Lorentz oscillators at low frequencies. The resultant lineshape is actually that of a single-pole Drude permittivity with $\omega_{a,0} = 0.094$ eV. (c) Spectral HTC from the initial (blue) and optimal (red) permittivities. Inset: zoomed-in profile of the optimal Re $\epsilon(\omega)$ near the near-field thermal frequency at 300 K, which is derived in the section "Wien Frequencies for Near-Field Energy Exchange between Real Materials".

There will generically be many local optima. One might consider a global optimization algorithm,53 but hundreds of free parameters prohibit any hope of convergence in such a large design space. Instead, we perform gradient-based local optimizations, which we run many times with different initial conditions, optimization parameters, and so on, and see consistent convergence to similar optimal HTC values and lineshapes, which suggests that we are approaching globally optimal values. Our gradient-descent-based local optimizations of eq 1 use hundreds of oscillators with frequencies $\omega_{a,i}$ spaced by 0.001 eV, and semianalytical expressions of the HTC gradients with respect to all parameters (cf. SM). In experimental optimizations, $\gamma_i = 0.004$ eV was found to offer the best optimal HTC levels, and we choose precisely this value for our optimizations (cf. SM). We allowed for the possibility of different materials for the two bodies, but the optimizations always converged on identical permittivity profiles, which is sensible, as alignment of resonant features likely enables maximum photon tunneling probabilities from one body to the other, and similar conclusion is also obtained in ref 40. To avoid poor-quality local optima, we typically run the optimizations in two stages: first, with a smaller number of parameters starting from a random initial guess, and then using "successive refinement"54 to polish the optimal solution with a very large number of parameters (cf. SM for more details). The optimizations typically converge within a few hundred iterations. Figure 1 depicts the initial and final permittivity distributions of a 400-oscillator optimization, with a random initial permittivity profile (blue) that converges to a smooth Drude-dominant profile by the end of the optimization. The ideal lineshape has a Drude pole ($\omega_{a,0} = 0$) with large oscillator strength, $\omega_{a,i} = 0.094$ eV, which is the dominant feature of the line shape. (The optimal oscillator strength scales with temperature, as discussed in the section "Wien Frequencies for Near-Field Energy Exchange between Real Materials".) The consistent simplicity of the optimal lineshape is further evidence that we are likely approaching a global optimum. The inset of Figure 1 shows the oscillator weights: there are typically a few other low-energy oscillators ($\omega_{a,i} < 0.1$ eV) with small but nonzero oscillator strengths, which provide small adjustments to the line shape to broaden the resonant bandwidth, with all remaining oscillator strengths converging to zero (cf. SM). The optimal lineshape parameters do not depend on the gap separation (in the near-field regime), which we explain in the following sections. The HTC from such simple lineshapes is approximately $2.6 \times 10^5$ W/(m$^2$K), a record level for 10 nm separations and 300 K temperatures.

Natural questions, then, are why the Drude lineshape is superior to more complex possibilities, why the optimal oscillator strength is 0.094 eV, and whether real materials can approach the optimal HTC values. In the next sections, we develop simple theoretical explanations of these questions. We start with the question of the optimal lineshape.

### IDEAL PERMITTIVITY PROFILE: DRUDE WITH SMALL $\epsilon_\beta$ AND MODERATE $G$

In this section we pinpoint the physical underpinnings for the optimal Drude lineshape. We focus on three ideas: why Drude is better than Drude–Lorentz or more complex lineshapes, why a small background permittivity is better than large ones and why moderate loss rates are also important. For the first two, minimal dispersion in the permittivity is the key controlling factor; it is not possible for a material to exhibit a resonant surface-plasmon permittivity of Re $\epsilon \approx -1$ over an infinite bandwidth (also due to causality constraints), but Drude materials with small background permittivities appear to offer the largest possible such bandwidths. We show below that they reach within 10% of a known global bound on minimal dispersion.55 With respect to the loss rate, moderate losses are optimal because there are tradeoffs between the source amplitudes and resonant amplifications that result in specific, moderate ranges of optimal loss rates. The prime importance of minimal dispersion also means that the optimal parameters are independent of gap separation, which does not alter the requirement of a large bandwidth of Re $\epsilon \approx -1$, nor the balance between source amplitudes and resonant amplification.

### SMALL BACKGROUND PERMITTIVITIES

The surface wave at an interface between a polaritonic material and air exhibits a modal dispersion relation for the wavenumber $\beta$ given by56

$$\beta^2 = \sqrt{\epsilon_{\beta} G}$$
The largest confinement, which occurs for the largest \( \beta \), occurs as \( \epsilon'(\omega) \) approaches \(-1\) from below, in the low-loss limit. This condition also holds for two-interface geometries, for example, metal–insulator–metal, where in the high-wavenumber limit the two interfaces effectively decouple.\(^5^8\) Moreover, one can show (cf. SM of ref \(^2^8\)) that the same condition of \( \text{Re} \epsilon'(\omega) \approx -1 \) is the condition at which peak HTCl occurs between planar layers in the low-loss limit, as the high confinement leads to the strongest resonant energy transfer. Thus, maximum HTCl requires the largest possible bandwidth over which \( \text{Re} \epsilon'(\omega) \approx -1 \) is the condition at which peak HTCl occurs between planar layers in the low-loss limit, as the high confinement leads to the strongest resonant energy transfer. Further quantitative support of the importance of Drude-type response and small background permittivity is given in Figure 3.

Figure 2 demonstrates why a Drude material with small background permittivity provide the largest bandwidth with \( \text{Re} \epsilon'(\omega) \approx -1 \). Three permittivity lineshapes are depicted: Drude with a small background permittivity (red), Drude with a large background permittivity (orange), and Drude–Lorentz with a small background permittivity (blue). The shaded gray region covers real permittivity values between \(-1.4\) and \(-0.6\) for a clear visual indication of bandwidth. The Drude–Lorentz bandwidth is quite small due to the nonzero transition frequency; \( \text{Re} \epsilon' \) ascends from \(-\infty\) at a nonzero frequency and does so much faster than a Drude material, exhibiting large dispersion and, thus, small bandwidth. A large background permittivity has a similar effect. As can be seen in Figure 2, as well as from eq 4, a large background permittivity increases the slope of the permittivity lineshape at every frequency, hence, increasing its dispersion and reducing its bandwidth. By contrast, the Drude lineshape with small background permittivity exhibits the least amount of dispersion and the largest bandwidth.

Further quantitative support of the importance of Drude-type response and small background permittivity is given in Figure 3. Figure 3a shows the modal dispersion relations\(^5^8\) between two half spaces with the three lineshapes, as in Figure 2, each with its optimal loss rate in terms of HTC. Figure 3b shows the spectral photon exchange, that is, the temperature-independent part of the HTC integrand. The close correspondence between (a) and (b) confirms the suitability of using modal analysis to interpret the modal and spectral components of HTC. With the given resonance type, Drude or Drude-Lorentz, and background permittivity \( \epsilon'_b \), the scattering loss rate is the other key parameter determining the lineshape and therefore the HTC. Unlike the loss rates in the many-oscillator representation of eq 8, for a single oscillator the optimal loss rate will be a nonzero value that helps mimic the many “lossless” oscillators of the Kramers–Kronig relation (which each have \( \delta \)-function losses at their transition frequencies). The optimal loss rates for the Drude and Drude-Lorentz models are computed by a grid search for each resonance type and \( \epsilon'_b \). Then we can compare the three types of lineshapes at their respective optimal loss rates, which reveals that the largest achievable \( \beta \) values are similar, indicating similar levels of spatial confinement on resonance. Yet one can see that the larger bandwidth of the small-background-permittivity Drude material provides a substantial advantage over the other materials.

Large, nonideal background permittivities usually occur in heavy elements or their compounds, which have many high-energy inner-shell electrons. This indicates the possible superiority of light materials, with small attendant background permittivities, a suggestion that is substantiated in our
The optimal frequency for \( \omega \), the green curves are the spectral photon exchanges, and the purple curves represent the bandwidth and gives best total HTC from plasmonic materials. The normalized temperature factor small of a loss rate results in overly narrow spectral bandwidths. A moderate loss rate (red) balances the effects of spatial confinement and spectral bandwidth and gives best total HTC from plasmonic materials.

Figure 4. Spectral dispersions and photon exchanges of Drude with \( \epsilon_b = 1 \) at three different loss rates, with frequencies normalized to plasma frequency \( \omega_p \). (a) Modal dispersions of gap surface waves. The permittivity with loss rate too large (green) suffers from poor spatial confinement. Smaller loss rates (purple) correspond to larger in-plane wavevector and better confinement on resonance, yet according to (b) the spectral photon exchanges, too small of a loss rate results in overly narrow spectral bandwidths. A moderate loss rate (red) balances the effects of spatial confinement and spectral bandwidth.

Figure 5. Spectral photon exchanges and spectral HTCs leading to Wien frequencies between different material models: blackbodies, bulk Drude materials, and 2D plasmonic materials, normalized to their respective \( \omega_{Wien} \). (a) Comparisons of spectral photon exchanges. In the case of blackbodies (blue), it is directly proportional to the DOS of propagating waves, whereas for bulk (red) and 2D (gray) material, photon exchange profiles are much narrower and are closely related to LDOS in the near field. Wien frequency analysis for blackbodies (b), bulk Drude and 2D materials (c). The red curves show the normalized temperature factors \( \frac{1}{2\pi} \frac{\partial H(\omega, T)}{\partial T} \), the green curves are the spectral photon exchanges, and the purple curves represent the product of the them, also defined as the spectral HTC. The peaks of the spectral HTC define \( \omega_{Wien} \) for each case.

The investigation of optimal real materials the section “Candidate Materials for Maximum Near-Field RHT”.

MODERATE LOSS

The second key factor of the optimal Drude lineshape is a moderate loss rate \( \gamma \). Figure 4 compares modal dispersions and spectral photon exchanges among three different choices of \( g = \gamma/\omega_p \), 0.01, 0.17, and 0.5, for the same single-Drude-pole line shape with \( \epsilon_b = 1 \). Large \( g \) broadens the spectral contributions, but gives few high-\( \beta \) states or small LDOS on resonance, seen from the dispersion. Meanwhile, small \( g \) provides huge LDOS on resonance, at the cost of very narrow peak-HTC bandwidth. The very large loss rates, while penalized less than very small loss rates, show suboptimal HTC due to their small peak values. The best integrated broadband response comes from intermediate values of \( g \), which equals 0.17 for \( \epsilon_b = 1 \). For \( \epsilon_b \) ranging from 1 to 13, optimal \( g \) and can range from 0.17 to 0.04, decreasing as \( \epsilon_b \) increases. Our result of moderate loss as optimal confirms coupled-mode predictions of such a trend.

WIEN FREQUENCIES FOR NEAR-FIELD ENERGY EXCHANGE BETWEEN REAL MATERIALS

The final optimal Drude parameter to explain is the plasma frequency \( \omega_p \), whose optimum is 0.094 eV for 300 K HTC. This optimal value is closely linked to the precise temperature spectrum of the sources under consideration, and in this section we derive a linear relation between the two.

For two macroscopic bodies in the far field, Wien’s displacement law states that the radiated energy of a blackbody is maximized at a frequency linearly proportional to its temperature. For two macroscopic bodies in the far field, Wien’s displacement law states that the radiated energy of a blackbody is maximized at a frequency linearly proportional to its temperature. The radiated energy is given by \( H = \left(1/4\pi^2\right) \int_0^\infty \Theta(\omega, T)S(\omega) \, d\omega \), where \( S(\omega) \) in this case is interpreted as a photon emissivity rate. A key distinction in the far-field case is that the term \( S(\omega) \) is proportional to the photon density of states, which scales as the square of frequency, \( \sim \omega^2 \) (ref 60). This quadratic scaling is critical to the determination of the Wien peak, blue-shifting the maximum-emission peak relative to the peak of the Planck distribution. One can similarly define a “Wien” peak for maximum far-field HTC, simply replacing \( \Theta(\omega, T) \) with \( \partial \Theta(\omega, T) / \partial T \). The optimal frequency for maximum HTC again scales linearly with temperature. One can generalize this further to radiative heat transfer between two bodies, with temperatures \( T_1 \) and \( T_2 \) yielding slight corrections to the linear relationship. The classical Wien’s Law is independent of separations as it relies only on energy transported through far-field channels. From Wien’s Law, the intuition has developed that the thermal wavelength is about 8–10 \( \mu m \) near 300 K temperatures, but this intuition is only valid.
for the far-field. In the near field, the wavelengths for peak thermal exchange are significantly longer.

In the near field, the spectral photon exchange (which replaces blackbody emissivity in the frequency integral) can exhibit extraordinarily large peaks due to the access to high-confinement near-field waves, but it cannot exhibit scaling \( \sim \omega^2 \). In contrast to the divergent density of propagating photon states, there is a known sum rule requiring that the integrated near-field local density of states must be finite.\(^{31,62}\) For a Drude material, the spectral photon exchange and the local density of states exhibit peaks at a resonant frequency \( \omega_r \), where the real part of the permittivity is \( -1 \), that is, \( \Re \epsilon(\omega_r) = -1 \), as seen in the red curve of Figure 5a. For room temperature and higher, the near-field radiative HTC and conductive HTC. (a) Wien frequencies for HTC at different operating temperatures. For bulk Drude materials in the near field, \( \omega_{\text{ff}} \) corresponds to 19 \( \mu \)m at 300 K. (b) Wien frequencies for RHT at different hot-body temperatures with selected cold-body temperatures at \( T = 0, 300, \) and 500 K. Blackbody Wien frequencies are always quite larger than those for near-field Drude materials in each of the cases. (c) Comparison of temperature scaling of HTCs of optimal near-field RHT and conductive heat transfer in the ballistic regime. Each dashed line is an HTC curve from an actual material optimized for temperature \( T = 30, 100, \) and 600 K.

Figure 6. Temperature-scaling laws for Wien frequencies for blackbodies in the far-field (blue) and bulk Drude materials in the near field (red) and for near-field radiative HTC and conductive HTC. (a) Wien frequencies for HTC at different operating temperatures. For bulk Drude materials in the near field, \( \omega_{\text{ff}} \) corresponds to 19 \( \mu \)m at 300 K. (b) Wien frequencies for RHT at different hot-body temperatures with selected cold-body temperatures at \( T = 0, 300, \) and 500 K. Blackbody Wien frequencies are always quite larger than those for near-field Drude materials in each of the cases. (c) Comparison of temperature scaling of HTCs of optimal near-field RHT and conductive heat transfer in the ballistic regime. Each dashed line is an HTC curve from an actual material optimized for temperature \( T = 30, 100, \) and 600 K.

The optimal resonance frequency \( \omega_r \) for near-field RHT is given by (cf. SM)

\[
\frac{h\omega_R^{\text{RHT}}}{k_B T} = 1.59
\]  

In the near field, the optimal Wien frequency is equivalent to the optimal Wien wavelength, regardless of whether the integrand is written in terms of frequency or wavelength. This stands in stark contrast to the far-field case, where the Wien peak is different in the two cases, due to the inverse relationship between the two that enters the differential in addition to the integrand itself.\(^{59}\) This does not occur in the near field thanks to the analytical structure of the HTC and heat-transfer expressions in which the integration parameter is effectively \( \ln \omega_r \) since \( d(\ln \omega) = d(\ln \lambda) \), there is no distinction whether parametrizing the radiation laws with \( \omega_r \) or \( \lambda \).

Figure 6 plots the optimal Wien frequencies, and their corresponding Wien wavelengths, for both near- and far-field HTC (a) and RHT (b). One can see the linear scaling relations that emerge in the near-field cases and the significantly smaller slopes that lead to much longer optimal wavelengths than for far-field blackbodies. Even for temperatures as high as 1000 K, the optimal resonance wavelength is 6 \( \mu \)m. For HTC at 300 K, the optimal plasma frequency of 0.094 eV translates to an optimal Wien frequency of 0.067 eV, which corresponds to an optimal operating wavelength of 19 \( \mu \)m.

\[\text{HTC} = \frac{(760 \text{ W/m}^2/\text{K})}{T}\]

for \( d = 10 \text{ nm} \). Thus, we have an explanation for the optimal plasma frequency and for the optimal HTC value, which is determined by the combination of bringing a large integrated spectral photon exchange as close as possible to zero frequency, where the Planck distribution peaks.

At high enough temperatures, for example, \( T \geq 130 \text{ K} \) for the \( d = 10 \text{ nm} \) configurations, these maximum near-field radiative HTCs exceed conductive HTCs in the ballistic regime under standard conditions for temperature and pressure.\(^{63}\) (cf. SM), as shown Figure 6c. Any given material (dashed lines) will not show linear temperature scaling itself, but the envelope of optimal materials (solid red line) exhibits exactly the predicted linear scaling.

A similar analysis can be done for radiative heat transfer (RHT) between two bodies of the same material at temperatures \( T_1 \) and \( T_2 \), with \( T_2 > T_1 \). For \( T_1 = 0 \) (an exact analog of the conventional Wien-law condition), the optimal Wien frequency \( \omega_1 \) for near-field RHT is given by (cf. SM)

\[
\frac{h\omega_1^{\text{RHT}}}{k_B T} = 1.59
\]  

for \( d = 10 \text{ nm} \). Thus, we have an explanation for the optimal plasma frequency and for the optimal HTC value, which is determined by the combination of bringing a large integrated spectral photon exchange as close as possible to zero frequency, where the Planck distribution peaks.

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\frac{h\omega_1^{\text{RHT}}}{k_B T} = 1.59
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\[
\frac{h\omega_1^{\text{RHT}}}{k_B T} = 1.59
\]  

for \( d = 10 \text{ nm} \). Thus, we have an explanation for the optimal plasma frequency and for the optimal HTC value, which is determined by the combination of bringing a large integrated spectral photon exchange as close as possible to zero frequency, where the Planck distribution peaks.

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DEEP-SUBWAVELENGTH, POSSIBLY ANISOTROPIC, STRUCTURED METAMATERIALS

Metamaterials, which exhibit effective properties different from their constituent materials, are a natural platform for potentially achieving maximal near-field HTC and RHT. Metamaterials with isotropic effective permittivities naturally fall under the umbrella of eq 8 and may exhibit HTC values close to the optimal $2 \times 10^5 \text{W/m}^2 \text{K}$ at 10 nm separations and 300 K temperatures but cannot surpass them. Yet anisotropic effective permittivities, as seen, for example, in hyperbolic metamaterials, are not subject to the isotropic representation of eq 8 and could potentially exhibit superior performance.

We performed an extensive set of computational optimizations of three classes of Maxwell–Garnett effective-medium metamaterials, namely, SM, and summarize our findings according to the class of structures under consideration:

1. Isotropic, periodic holes: the materials retain isotropic optical properties. With air fill fraction represented by $f$, the effective permittivity is:
   \[
   \epsilon_{\text{eff}} = \frac{(1 - f)\epsilon + 1 + f}{1 - f + (1 + f)\epsilon}
   \]  
   (13)
as detailed in the SM, reducing the electronic density of plasmonic materials brings down both the effective $\epsilon_b$ and effective frequency $\omega_b$. For nonideal materials with $\epsilon_b$ and $\omega_b$ that are too high, isotropic air holes can greatly help. They cannot improve materials that are already ideal.

2. Periodic cylinders: cylinders oriented perpendicular to the surfaces lead to a difference in the permittivities along the ordinary and extraordinary axes. The ordinary-axis permittivity is the same as that for isotropic periodic holes, and many resonance properties are similar. There can be a little improvement from anisotropic hyperbolic bands, but the effect is minor and not obvious. Apart from the anisotropic hyperbolic bands, such patterning scheme offers effects that are similar to those from isotropic air holes, as shown in the SM, but is of more practical interest due to fabrication considerations.

3. Thin-film stacks (hyperbolic metamaterials): deep-subwavelength, periodic multilayer stacks lead to hyperbolic dispersion bands. However, the hyperbolic resonances are far less tightly confined to the surface compared to plasmon or phonon surface polaritons, resulting in smaller HTC. The thin-film stacks are inferior to periodic cylinders for ideal and nearly ideal materials. If one starts with materials with nonideal bulk parameters, such as highly doped Si with both $\epsilon_b$ and $\omega_b$ too high, such patterning can be optimized to offer HTC improvements, yet cannot outperform the ideal bulk materials.

We refer to the SM for a detailed effective-medium theory (EMT) description of the effective permittivities arising from these patterning schemes and a comparison of their optimal HTC values. In the section "Candidate Materials for Maximum Near-Field RHT" we compare estimates of optimal nanostructured materials to optimal bulk materials. Our central finding is that patterning can provide marginal improvements but at the expense of significant fabrication complexity due to the tiny required feature sizes. Moreover, all of the effective-medium-theory values become approximate (and likely overestimates) at the small separation distances of primary interest, further diminishing the possible improvements via such patterning.

2D MATERIALS

Reduced material dimensionality leads to qualitatively different polaritonic response. The plasmon-polariton dispersion relation for a 2D plasmonic material, for example, is quite different from that of a bulk plasmonic half space, with the resonant frequency scaling as the square root of the wavenumber, $\omega_i \sim \sqrt{\beta}$, instead of asymptotically approaching a constant value. Yet we still find that optimal 2D materials exhibit narrowband RHT response relative to blackbodies, offering many similarities to their optimal bulk counterparts. In this section, we carry out similar numerical optimizations and analyses as those in the bulk case and comparatively present the results for 2D materials by identifying the direct analogs and highlighting the differences with the optimal bulk Drude materials.

For a 2D material, causality implies a conductivity of the form (cf. SM),

\[
\sigma_{2D} = ie\omega_b \sum_{i=1}^{N} \frac{\omega_{/2}}{\omega_{/2} + \omega_{/2}^{2} + i\omega_{/2}^{2}}
\]  
(14)
which is the analog of the bulk-material representation, eq 8. The $t$ is a dummy-variable thickness (assumed to be 1 nm throughout) such that the $\omega_i$ have dimensions of frequency is canceled in the sum rule for $\omega_b$, leading to the Drude–Lorentz terms (with nonzero $\omega_0$), and the latter two classes, in addition, also possess 2D plasmons/intragap transitions, leading to Drude terms (with $\omega_0 = 0$). By the same process as for bulk materials, we use gradient descent to optimize over the set of conductivities represented by eq 14, and we find analogous results: the optimal profiles are dominated by a single-pole conductivity, as shown in Figure 7(a), and compared to the initial guess, the optimal profiles provide spectral HTC contributions at a rather broad range of low-energy frequencies.
Figure 10. HTC.s from periodic cylindrical-hole patterning of many materials, as a function a feature size for a unit cell fixed at 50 nm length and width. For ideal materials (metal, ITO, and CdO at their optimal carrier concentrations), the unpatterned HTC (right-most axis) reaches at least half of the best patterned HTC levels. For materials with much higher than ideal carrier concentrations (n-type InP, n-type InAs, n-type Si, Zn$_{0.982}$Ga$_{0.018}$O), patterning can greatly help. Patterning does not help polar dielectrics (SiC). Solid triangles indicate materials with experimentally measured permittivity data at the required carrier concentrations, while hollow triangles indicate the need for such measurements. All finite-feature-size data uses effective-medium theory and may overestimate HTC, further strengthening the case for ideal materials without patterning.

as shown in Figure 7b. Although the dominant oscillator is not strictly Drude type, its frequency is nearly zero ($\approx 10 \text{ meV}$). The other oscillators either have very small amplitudes $\omega_{i b}$ if their oscillator frequencies are small or have exactly $\omega_{i b} = 0$ if their oscillator frequencies are large. The optimal HTC level is $2.7 \times 10^5 \text{ W/(m}^2\text{K)}$, larger even than the optimal bulk-material HTC. Even for a completely 2D plasmonic material, that is, with single 2D Drude oscillator optimized for $d = 10 \text{ nm}$ so that $\omega_{i 0} = 0.24 \text{ eV}$, HTC can be as large as $2.4 \times 10^5 \text{ W/(m}^2\text{K)}$, as highlighted by the blue marker in Figure 7c. For every other $d$, the optimal Drude oscillator amplitudes $\omega_{i b}$ and, hence, 2D carrier concentrations, $n_{2D}$, need to be reoptimized in order to match the optimal gap surface wave modal dispersions, as opposed to being essentially constant in the case of bulk Drude materials.

The bulk-material intuition carries over to 2D materials: the Drude pole or Drude—Lorentz pole with negligible $\omega_{i 0}$ (<<0.1 eV) is ideal because it maximizes the bandwidth of large RHT response, and the optimal loss rate is a moderate value that trades off strong confinement (low loss) with large bandwidth (high loss). In addition, 2D material performances are also affected by the substrate. Substrates with refractive index higher than that of vacuum lead to decreased confinement (cf. SM) and are therefore nonideal. The Wien frequencies for RHT and HTC are quite similar to those of bulk materials, with a slight blue shift due to the wider bandwidth arising from the dispersion of two sheets of 2D materials at the optimal loss rate, as shown in Figure 5a,c. We include a plot of the optimal 2D-material Wien frequencies in the SM.

### CANDIDATE MATERIALS FOR MAXIMUM NEAR-FIELD RHT

Here we synthesize the optimal bulk- and 2D-material results of the previous sections to identify the best candidate materials for maximal HTC and RHT. For bulk-material HTC at 300 K, we found three key properties: Drude-like response with resonant wavelengths of $\approx 19 \mu\text{m}$, small background permittivity and moderate loss rates ($g \approx 0.04$ to 0.17, decreasing as $\epsilon_i$ increases, detailed in SM). Loss rates and background permittivities can be tabulated for a wide variety of materials. In Figure 8, we plot HTC level curves as a function of resonant frequency $\omega_i$ and background permittivity $\epsilon_{b 0}$ overlaid with a wide variety of possible materials. Noble metals (Ag, Al) and alternative plasmonic materials such as GZO (Ga-doped ZnO) and Dy-doped CdO have resonant frequencies that are too large, while semiconductors such as Si and GaAs can be doped to the right resonant frequencies but exhibit background permittivities that are too large. Lightly doped TCOs and III-nitrides are particularly promising material classes that present themselves as potentially optimal.

Figure 9 compares the theoretical HTC values for many bulk and 2D materials, as well as the optimal possible values, which are shown as the dashed (bulk) and dotted (2D material) lines. The previous theoretical state-of-the-art for unpatterned bulk materials, using SiO$_2$, is depicted with orange markers. Doped III–V$_i$s, such as GaAs and InP, even with their high background permittivities, can already show enhancements beyond SiO$_2$, given published permittivity data. Yet, the real gains to be had are with the lighter materials, such as AlN, CdO, and ITO. If these materials can be doped to the optimal carrier concentrations listed in Figure 9, they can exhibit 5X enhancements beyond the current state-of-the-art. (The optimal carrier concentrations tend to range from 3 to $7 \times 10^{18} \text{ cm}^{-3}$, multiplied by $\epsilon_i m_{e i} / m_u$.) Patterning in suboptimal materials, such as n-type InP and n-type Si, can lead to slight further enhancements, discussed below, though the feasibility of effective-medium theory for describing such response is dubious at separations below 50 nm for the given choice of temperature and unit cell size, as indicated by the open markers. 2D materials are particularly promising: purely plasmonic response can exhibit broad resonant bandwidth and strong confinement at the same time. For example, graphene with Fermi level $E_F = 0.4 \text{ eV}$ (optical conductivity from ref 88) is shown to exhibit near-optimal HTC values at separations on the order of 100 nm, though a key distinction from the optimal bulk materials is that the optimal oscillator amplitude $\omega_{i b}$ and therefore, the optimal 2D carrier concentration $n_{2D}$ varies with the separation distance.
Agnostic of the bandgap and electronic dispersion of the 2D materials, the optimal ω₀ and the corresponding maximal HTCs can be identified for each d, as shown in Figure 7c and SM. These HTCs along the dotted gray line in Figure 9 are higher than those from any other materials. For linear Dirac electronic dispersion, as in graphene, the optimal carrier concentration optimal n_{2D} is \(9 \times 10^{11} \text{ cm}^{-2} \times \left(\frac{d}{100 \text{ nm}}\right)^2\). Graphene holds potential for optical response over a great range of electromagnetic spectrum from radio waves to visible frequencies,\(^{77}\) and its optical conductivity \(\sigma_{2D}(\omega)\) is well-studied in literature, with the infrared spectral range dominated by intraband transitions.\(^{71,88,89}\) making it the exemplary 2D material in our study. However, as the optical properties of other 2D plasmonic materials, 2D semiconductors, and semimetals, in particular, are better characterized, it is likely that they may offer similar or superior performance to graphene.

Figure 10 confirms the pros and cons of metamaterial patterning. In a previous section we found that periodic cylindrical holes offer strong performance in a lithography-compatible form factor, and in Figure 10 we consider the electromagnetic spectrum from radio waves to visible frequencies,\(^{77}\) and the optical conductivity \(\sigma_{2D}(\omega)\) is well-studied in literature, with the infrared spectral range dominated by intraband transitions.\(^{71,88,89}\) making it the exemplary 2D material in our study. However, as the optical properties of other 2D plasmonic materials, 2D semiconductors, and semimetals, in particular, are better characterized, it is likely that they may offer similar or superior performance to graphene.

**ASSOCIATED CONTENT**

**Supporting Information**

The Supporting Information is available free of charge at https://pubs.acs.org/10.1021/acsphotonics.0c01176.

Permittivity and conductivity representations via discretized Kramers–Kronig relations, setup of oscillator-strength optimization of HTC, results from oscillator-strength optimizations, derivations of near-field Wien frequencies, comparison between optimal radiative HTC and conductive HTC, HTC from three types of effective-medium metamaterials, optical properties of 2D plasmonic materials and their near-field HTCs, Wien frequencies for 2D plasmonic materials, 2D plasmonic materials with different substrate refractive indices, gap distance dependence of optimal \(\omega_0\) and \(n_{2D}\) for 2D plasmonic materials (PDF)

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Supplementary Material: Optimal materials for maximum near-field radiative heat transfer

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I. PERMITTIVITY AND CONDUCTIVITY REPRESENTATIONS VIA DISCRETIZED KRAMERS–KRONIG RELATIONS

In this section we show that starting only with the Kramers–Kronig (KK) relations (in turn, dependent only on causality and basic asymptotic-frequency assumptions), a general representation of any permittivity is that of a summation of Drude–Lorentz oscillators. We start with the KK relation, one version of which relates the real part of the permittivity at any one frequency to a principal-value integral of the imaginary part:

\[
\text{Re} (\epsilon (\omega)) = 1 + \frac{2}{\pi} \text{P.V.} \int_0^\infty \frac{\omega' \text{Im} \epsilon (\omega') d\omega'}{\omega'^2 - \omega^2}.
\] (S1)

One can see that the integrand already has a passing resemblance to a lossless Lorentz–Drude oscillator with oscillator frequency \( \omega' \), but it may not be immediately obvious how to think about the \( \omega' \text{Im} \epsilon (\omega') \) term in the numerator. The key is to use a known sum rule for the imaginary part, which is [1]:

\[
\int_0^\infty \omega' \text{Im} (\epsilon (\omega')) d\omega' = \frac{\pi \omega_p^2}{2}.
\] (S2)

where \( \omega_p \) is the plasma frequency, which is related to free carrier concentration through Eq. (3) in the main text. The sum rule implies that \( \omega' \text{Im} \epsilon (\omega') \) can be discretized into local basis functions whose amplitudes are constrained by the
constant on the right-hand side of Eq. (S2). As one example, we consider the limit of perfectly localized delta-function basis functions for the decomposition:

$$\omega' \Im(\epsilon(\omega')) = \frac{\pi \omega_p^2}{2} \sum_i c_i \delta(\omega' - \omega_i).$$

(S3)

The constant $\pi \omega_p^2/2$, in tandem with the sum rule of Eq. (S2), ensures that basis-function coefficients that determine the distribution of $\omega' \Im(\epsilon(\omega'))$ must sum to 1:

$$\sum_i c_i = 1.$$  

(S4)

Inserting this representation of the imaginary part into the KK relation for the real part, Eq. (S1), we find:

$$\Re(\epsilon_{KK}(\omega)) = 1 + \sum_i \frac{c_i \omega_p^2}{\omega_i^2 - \omega^2},$$

(S5)

where the superscript “KK” has been added to distinguish from a Drude–Lorentz representation below. Hence in the limit of perfectly localized basis functions, the KK relations imply a permittivity whose real part satisfies Eq. (S5), and whose imaginary part (rewriting Eq. (S3)) satisfies

$$\Im(\epsilon_{KK}(\omega)) = \frac{\pi \omega_p^2}{2} \sum_i \frac{c_i \delta(\omega - \omega_i)}{\omega_i}.$$  

(S6)

It is straightforward to show that the KK representation of Eqs. (S5,S6) is equivalent to a lossless Drude–Lorentz (DL) representation. Consider a permittivity comprising a summation of Drude–Lorentz oscillators:

$$\epsilon_{DL}(\omega) = \left(1 + \sum_i \frac{c_i \omega_p^2}{\omega_i^2 - \omega^2 - i\gamma\omega}\right).$$

(S7)

In the limit of lossless oscillators, we take $\gamma \to 0$ from above. To evaluate the DL expression in this limit, considering the real-line integral of $\omega_i$ gives an important identity: $\lim_{\gamma \to 0} \left[1/(x + i\gamma)\right] = 1/x - i\pi\delta(x)$, in which case the DL expression simplifies to:

$$\lim_{\gamma \to 0} \epsilon_{DL}(\omega) = 1 + \sum_i \frac{c_i \omega_p^2}{\omega_i^2 - \omega^2} + i\pi \frac{\delta(\omega - \omega_i)}{2\omega_i},$$

(S8)

where the last equality uses the fact that $\omega_i \geq 0$ to remove an additional delta-function term proportional to $\delta(\omega + \omega_i)$. Inserting the right-hand side of Eq. (S8) into the DL representation gives:

$$\lim_{\gamma \to 0} \epsilon_{DL}(\omega) = 1 + \sum_i \frac{c_i \omega_p^2}{\omega_i^2 - \omega^2} + i\pi \frac{\sum_i c_i \delta(\omega - \omega_i)}{2\omega_i} = \epsilon_{KK}(\omega).$$

(S9)

Hence, any KK material can be represented as a (possibly infinite) sum of Drude–Lorentz oscillators.

A similar KK representation and sum rule [2] yields an analogous Drude–Lorentz representation for arbitrary 2D conductivities (with dummy thickness variable $t$ inserted for dimensionality compatibility):

$$\sigma(\omega) = i\epsilon_0 \omega t \left[\sum_i \frac{c_i \omega_p^2}{\omega_i^2 - \omega^2} + i\pi \frac{\sum_i c_i \delta(\omega - \omega_i)}{2\omega_i}\right] = \lim_{\gamma \to 0} \sigma_{DL}(\omega).$$

(S10)

II. SETUP OF OSCILLATOR-STRENGTH OPTIMIZATION OF HTC

Given the general permittivity/conductivity expressions derived in the previous section, arising from the Kramers–Kronig relations, the optimal material that maximizes HTC is the one whose oscillator strengths satisfy the optimization problem:

$$\begin{align*}
\text{maximize} & \quad \text{HTC} \\
\text{subject to} & \quad \omega_{a,i} \geq 0, \omega_{0,i} \geq 0.
\end{align*}$$

(S11)
To reduce the dimensionality of the problem, we can select a finite number of oscillators $N$ and fix their intrinsic frequencies $\omega_{0,i}$ over a one-dimensional grid, leaving only the oscillator strengths $\omega_{a,i}$ to be optimized. (By fixing $\omega_{0,0} = 0$ we ensure the first oscillator is the Drude type, and any other $\omega_{0,i} \neq 0$ represents the oscillator frequencies of Drude-Lorentz oscillators.) We can then optimize over the $\omega_{0,i}$ via gradient descent, converging on local optima and re-running the optimizations many times to ensure discovery of solutions at or very near the global optima.

![Graph](image.png)

**FIG. S1:** Results of numerical experiments for the choice of $\gamma$ in the optimizations, shown in terms of the optimal HTCs from multi-oscillator optimizations with different choices of $\gamma$. $\gamma$ in the range $0.002 \sim 0.008$ eV leads to HTCs higher than $2.5 \times 10^5$ W/(m$^2$K), and is thus used in later optimizations.

To compute the gradients, we start with the modal photon exchange function:

$$\xi(\omega, \beta) = \frac{4(\text{Im} r)^2 e^{2ik_0,zd}}{|1 - r^2 e^{2ik_0,zd}|^2}, \quad (S12)$$

and the interface reflectivity:

$$r(\omega, \beta) = \frac{k_{0,z} \epsilon - k_z}{k_{0,z} \epsilon + k_z}, \quad (S13)$$

where $k_{0,z} = \sqrt{\frac{\omega^2}{c^2} - \beta^2}$ and $k_z = \sqrt{\frac{\epsilon \omega^2}{c^2} - \beta^2}$ are respectively the z-component of wavevectors in air and in material. The gradient of the modal exchange function is given by

$$\frac{d\xi(\omega, \beta)}{d\omega_{a,i}} = 2 \text{Re} \left[ \frac{d\xi(\omega, \beta)}{dr} \frac{dr(\omega, \beta)}{d\epsilon} \frac{d\epsilon}{d\omega_{a,i}} \right], \quad (S14)$$

where

$$\frac{d\xi(\omega, \beta)}{dr} = \frac{e^{2ik_0,zd}(r - r^*) (1 - ry^*) e^{2ik_0,zd}}{2(1 - r^* e^{2ik_0,zd})(1 - ry e^{2ik_0,zd})^2}, \quad (S15)$$

$$\frac{dr(\omega, \beta)}{d\epsilon} = \frac{2k_z k_{0,z}}{(k_{0,z} \epsilon + k_z)^2}, \quad (S16)$$

$$\frac{d\epsilon}{d\omega_{a,i}} = -\frac{2\omega_{a,i}}{\omega^2 - \omega_{0,i}^2 + i\omega \gamma_i}. \quad (S17)$$

The HTC gradients with respect to each oscillator strength are calculated by numerical integration:

$$\frac{d\text{HTC}}{d\omega_{a,i}} = \frac{1}{4\pi^2} \int_0^\infty \frac{d\Theta(\omega, T)}{dT} \int_0^\infty \frac{d\xi(\omega, \beta)}{d\omega_{a,i}} \beta d\beta d\omega. \quad (S18)$$
How are the loss levels (scattering rates) $\gamma$ of these basis functions chosen? Before a large number of optimizations can be run, numerical experiments can be done to fix the range plausible $\gamma$. With a fixed grid spacing $\delta = \omega_{0,i+1} - \omega_{0,i}$, we run test optimizations to analyze the effects of $\gamma$ values on the optimal HTCs, results summarized in Fig. ???. It is from these results that $\gamma$ range of $0.002 \sim 0.008$ eV, leading to higher than $2.5 \times 10^5$ W/(m$^2$K) HTCs in the experiments, is identified to potentially maximize HTC. The optimization results shown throughout are based on such choice of $\gamma$ range.

III. RESULTS FROM OSCILLATOR-STRENGTH OPTIMIZATIONS

![Fig. S2: (a) The initial guess (blue) and optimal permittivity profile (red) of one representative 100-oscillator optimization, with oscillator frequency $\omega_{0,i}$ sampled from 0 to slightly beyond 0.4 eV. Inset shows the corresponding oscillator amplitudes $\omega_{n,i}$. (b) Spectral HTC from the initial (blue) and optimal (red) permittivities. Inset: zoomed-in profile of the optimal $\epsilon_r$ near the optimal  $\omega_i$.](image)

In the main text, we presented the results from a 400-oscillator optimization where grid spacing of $\omega_{0,i}$ is 0.001 eV and $\gamma = 0.004$ eV, which clearly shows that (1) the Drude-dominant lineshape is pivotal, and that (2) multiple Drude-Lorentz oscillators can be useful to broaden the resonance bandwidth by flattening the range of $\epsilon \approx -1$ near the optimal $\omega_i$.

At lower resolutions and the same loss levels ($\gamma = 0.004$ eV), it becomes obvious that the individual oscillators with oscillator frequency $\omega_{0,i}$ near the optimal $\omega_i$ tend to create small bumps in the permittivity profile and in spectral HTC, as can be demonstrated in a 100-oscillator optimization where $\omega_{0,i}$ is sampled from 0 to 0.4 eV with grid spacing 0.004 eV. From a random starting point where all $\omega_{n,i} \neq 0$, the optimization result has the largest non-zero amplitude for the Drude oscillator and only a few small amplitudes for Drude-Lorentz oscillators at low frequencies. Such features from low-resolution results are retained in higher-resolution optimizations, and can be useful to help the latter better converge to high-quality local optima via successive refinement. The inset in Fig. S2(a) shows that every $\omega_{n,i}$ with oscillator frequency $\omega_{0,i} > 0.1$ eV tends to vanish. Hence the resultant lineshape is predominantly that of a single-pole Drude permittivity with $\omega_{\infty} = \omega_p = 0.094$ eV superimposed by small bumps near $\omega_i$ which flatten the range of $\epsilon \approx -1$ and thus broaden the resonance bandwidth. Furthermore, the bumps around the optimal $\omega_i$, due to the coarse sampling of $\omega_{0,i}$ and the small loss level, can be smoothed out at higher resolution, as is apparent from the optimization results in the main text.

IV. DERIVATIONS OF NEAR-FIELD WIEN FREQUENCIES

In this section, we derive the optimal plasma frequency, or related resonance frequency, of the Drude materials that are optimal for HTC. Using the optimal permittivity lineshape argued in the main text, i.e. Drude-type with $\epsilon_b = 1$, the only free parameter in fixing $\epsilon(\omega)$ is the plasma frequency $\omega_p$, or the resonance frequency $\omega_i$. This optimal resonance frequency problem is quite similar to the Wien frequency argument in blackbody radiation. For largest spectral contribution to HTC between blackbodies, the Wien frequency $\omega_W^{\text{HTC}}$ maximizes $\frac{d\Theta(\omega,T)}{dT} B(\omega,T)$ where the
spectral radiance \( B(\omega, T) \) is given by
\[
B(\omega, T) = \frac{\omega^2}{4\pi^2 c^2} \frac{h\omega}{e^{h\omega/k_B T} - 1}.
\]
Setting \( x = \frac{h\omega}{k_B T} \) and taking its derivative to 0, the maximum is found to solve the equation
\[
(x - 4)e^x + x + 4 = 0,
\]
which has the positive solution 3.83. For Wien frequency for RHT \( \omega_{\text{RHT}}^W \), which maximizes \( (\Theta(\omega, T_2) - \Theta(\omega, T_1)) B(\omega, T) \), and taking the cold-body, or environment temperature \( T_1 = 0 \), the corresponding equation is
\[
(x - 3)e^x + 3 = 0,
\]
which has the positive solution 2.82. Take the radiation from the sun for example: with \( T_2 = 5778 \) K, one finds \( \omega_{\text{RHT}}^W = 1.91 \) eV, which is the well-known Wien frequency from solar radiation. Parametrizing Planck’s law in Eq. (S19) by wavelength \( \lambda \) gives a different Wien frequency \( \omega_{\text{RHT}}^W = 1.40 \) eV.

For near-field Wien frequencies, the major contribution comes from gap surface waves (tunnelling evanescent waves) instead of propagating plane waves. This is apparent in the much sharper spectral photon exchange of the “near field, Drude” configuration than the “far field, blackbody” configuration, and lead to Wien frequencies significantly smaller than those of the blackbodies. By normalizing the frequencies in the HTC integral against the resonance frequency \( \nu = \omega/\omega_r \), the HTC is given by
\[
\text{HTC} = 1 - \frac{\int_0^\infty \frac{d\Theta(\nu, T)}{dT} \omega_r \int_0^\infty \xi(\nu, \beta) \beta d\beta d\nu}{S(\nu)}.
\]
\( S(\nu) \) is now independent of \( \omega_r \) and sharply peaks exactly at \( \nu = 1 \), i.e. \( \omega = \omega_r \). We therefore arrive at a single-parameter optimization aiming to maximize \( \frac{d\Theta(\nu=1, T)}{dT} \omega_r \) over \( \omega_r \). The optimization simplifies to solving
\[
(x - 3)e^x + x + 3 = 0,
\]
leading to \( x = \frac{h\omega}{k_B T_2} = 2.57 \). As for RHT in the near field, with the cold-body temperature \( T_1 = 0 \), the objective function now is \( (\Theta(\nu = 1, T_2) - \Theta(\nu = 1, T_1 = 0)) \omega_r = \Theta(\nu = 1, T_2) \omega_r \), leading to
\[
(x - 2)e^x + 2 = 0,
\]
which has a solution \( x = \frac{h\omega}{k_B T_2} = 1.59 \).

For other non-zero \( T_1 \), similar equations can be derived and solved, and the results are plotted in Fig.6(b) of the main texts.

Just like the far-field case for blackbodies, the near-field Wien laws conclude that the hotter the temperature, the bluer the peak spectral thermal radiation, owing to the Planck distribution \( \Theta(\omega, T) \). The linear scaling relation with temperature is retained in the near field, which is a signature of thermal exchange via radiation, in contrast to conduction, whose scaling relation we show in the next section. The differences between the density of states of propagating plane waves in the far field and the local density of states of the gap surface waves in the near field manifest themselves as the different numerical factors in these transcendental equations, which result in much smaller solutions as Wien frequencies in the near field. Fortuitously, the equations for the near-field case are agnostic whether parametrizing the RHT or HTC integral with \( \omega \) or \( \lambda \), preventing the ambiguity of the spectral location of Wien peak which occurs in the far-field case.

V. COMPARISON BETWEEN OPTIMAL RADIATIVE HTC AND CONDUCTIVE HTC

Given the optimal loss rate for a given separation distance, \( \omega_{\text{RHT}}^W \) derived above dictate the optimal \( \omega_p \) at every temperature, and lead to optimal near-field radiative HTC values that scale linearly with temperature as described by Eq. (9) in the main text, which we include here:
\[
\text{HTC}_{\text{rad}} = (760 \text{ W/m}^2/\text{K}^2) T.
\]
For conductive HTC for the plane-plane configuration, gap separations on the order of 10nm are well below the mean free path in air 68 nm [3], thus it is safe to assume ballistic conductive heat transfer: no collision of gas molecules
FIG. S3: Optimal loss rates $g$ of bulk plasmonic materials with $\epsilon_b = 1$ at a range of $d$, which is a fixed value, confirming that the optimal bulk material parameters are unaffected by the given range of $d$. Optimal HTC levels scale as $\sim \frac{1}{d^2}$.

FIG. S4: Parametric optimization of optimal $g$ for a list of practical $\epsilon_b$. Optimal $g$ decreases as $\epsilon_b$ increases.

happen in the air gap, and the only collisions occur on the air-material interface. The conductive HTC for such configuration is [4]:

$$\text{HTC}_{\text{cond}} = \frac{3}{2} k_B n_g v_z,$$  \hspace{1cm} (S26)

where $v_z = \sqrt{\frac{k_B T}{m}}$ is the mean velocity of particles normal to the plates, and $m$ is single-particle mass. Assuming particle number density in air under standard conditions for temperature and pressure, $n_g = 2.5 \times 10^{25} \text{ m}^{-3}$, the
conductive HTC scales with the square root of $T$ as

$$\text{HTC}_{\text{cond}} = \left(8786 \text{ W/m}^2/\text{K}^{3/2}\right) \sqrt{T}.$$  \hfill (S27)

At lower temperatures, conductive heat transfer dominates, whereas near-field RHT can surpass conductive heat transfer rates at high enough temperatures. For the gap separation of 10 nm, the two HTC\-s cross at $T = 134 \text{ K}$.

VI. PARAMETRIC OPTIMIZATIONS OF THE OPTIMAL LOSS RATES

Recognizing that the optimal plasmonic loss rates balances both effects of bandwidth of gap surface resonances and of on-resonance density of states, a quantitative analysis incorporating both effects can be challenging. However, parametric sweeping of loss rates can be helpful for given choices of geometry and material parameters. For two bulk objects with changing gap separations, only the amplitude of the spectral photon exchanges are different, and their bandwidths are fixed for fixed loss rate, and all the optimality conditions, especially $\omega_p$ and $g$, are the same. Figure S3 is a result from parametric optimization of loss rates given $\epsilon_b = 1$ and $\omega_p$ dictated by Wien frequencies, confirming that the optimal loss rates is a fixed value for the range of gap distances.

In practical sense, materials with $\epsilon_b \neq 1$ are used more often in near-field RHT. As Fig. S4 shows, higher $\epsilon_b$ tends to lead to lower optimal $g$, as the former lowers resonance bandwidth in spectral photon exchange, requiring larger resonance strength provided by smaller $g$. Meanwhile, given the practical range of $g$, the smaller $\epsilon_b$, the more $g$ tends to affect HTC\-s.

![FIG. S5: Modal photon exchanges of ITO](image_url)

FIG. S5: Modal photon exchanges of ITO (a) in bulk, unpatterned form, (b) with periodic and deep-subwavelength patterning of isotropic holes, (c) with periodic and deep-subwavelength patterning of cylinders in z-direction, and (d) with periodic and deep-subwavelength patterning of thin-film stacks in z-direction (hyperbolic metamaterials). The volume fill ratio of air is 0.8 for all the patterned materials.
FIG. S6: HTCs from periodic isotropic air-hole patterning of many materials, as a function a feature size for a unit cell fixed at 50 nm length and width. For ideal materials (metal, ITO, CdO at their optimal carrier concentrations), the unpatterned HTC (right-most axis) reaches at least half of the best patterned HTC levels. All the HTCs of the best patterned cases do not surpass the upper bound provided by the causality constrained numerical optimizations. For materials with much higher than ideal carrier concentrations (n-type InP, n-type InAs, n-type Si, Zn$_{0.982}$Ga$_{0.018}$O), patterning can greatly help. Polar dielectrics (for example, SiC) are rarely helped by such patterning. Solid triangles indicate materials with experimentally measured permittivity data at the required carrier concentrations, while hollow triangles indicate the need for such measurements. All finite-feature-size data uses effective-medium theory and may overestimate HTC. Even though under some feature sizes, such patterning scheme is better than in-plane patterning of 2D cylindrical holes shown in the main text, these data are of more theoretical interest than practical implication as fabrication of 3D isotropic holes can be complicated.

VII. HTC FROM THREE TYPES OF EFFECTIVE-MEDIUM METAMATERIALS

Many insights about the effective-medium patterned materials can be gained by examining in tendem the homogenized material parameters and the corresponding modal photon exchanges. Here we choose ITO ($\epsilon_b = 3.8$) at its optimal carrier concentration ($n = 5.9 \times 10^{18} cm^{-3}$) as an example. As can be seen from Fig. S5(a), for the bulk, unpatterned ITO, the optimal $n$ guarantees alignment of strong gap surface resonance at the optimal $\omega_r$, namely $\omega_{Wien}$. But because of the non-unity $\epsilon_b$, its relative bandwidth, $\Delta \omega \omega_r$ ($\Delta \omega$ here is the full width at half of the maximal spectral HTC), is not as broad as it would optimally be based only on causality. Broader bandwidth can be expected from inclusions of air holes (or air cylinders, air layers) which reduces the effective $\epsilon_b$ by reducing the effective electron density.

According to Maxwell–Garnett effective-medium theory, an air fill fraction $f$ in a medium with permittivity $\epsilon$ yields an effective permittivity of

$$\epsilon_{\text{eff}} = \frac{(1-f)\epsilon + 1 + f}{1 - f + (1+f)\epsilon} \epsilon. \tag{S28}$$

From Fig. S5(b), the surface resonance frequency is lowered compared to the unpatterned case in (a), due to smaller $\omega_{p,\text{eff}}$, and the relative bandwidth is broadened, due to smaller $\epsilon_{b,\text{eff}}$. Although $\omega_r$ becomes misaligned with $\omega_{Wien}$ after patterning, the overall HTC is higher than that of the unpatterned ITO, thanks to the reduction in $\epsilon_{b,\text{eff}}$.

Periodic patterning of cylinders along $z$-direction, the in-plane patterning version of holes, has effective permittivity along the ordinary axis the same as Eq. (S28):

$$\epsilon_{o,\text{eff}} = \frac{(1-f)\epsilon + 1 + f}{1 - f + (1+f)\epsilon} \epsilon, \tag{S29}$$

and along the extraordinary axis:

$$\epsilon_{e,\text{eff}} = (1-f)\epsilon + f. \tag{S30}$$
Anisotropy leads to hyperbolic resonances near 0.04 ∼ 0.05 eV, as shown by Fig. S5(c), yet other than that, much of the behavior is similar to that from isotropic, periodic hole patterning. This modal photon exchange corresponds to the data point of ITO at feature size 25 nm in Fig. 10 of the main text. The enhancement of HTC here, about a factor of 1.4, is close to that from the optimal feature size.

Hyperbolic metamaterials, in this case thin stacks of material and air arranged periodically in z-direction, can be homogeneously characterized by

\[
\epsilon_{o,\text{eff}} = (1 - f)\epsilon + f, \quad (\text{S31})
\]

\[
\epsilon_{e,\text{eff}} = \frac{\epsilon}{1 - f + f\epsilon}, \quad (\text{S32})
\]

along ordinary and extraordinary axes respectively. For such configuration, thermal exchanges occur predominantly through hyperbolic resonances, shown by Fig. S5(d), whose confinement to the planar-planar surfaces is fairly small. Thus even with a broad resonance bandwidth, its HTC is nowhere near that from the above two types of effective-medium metamaterials, and even smaller than that of the unpatterned ITO.

We chose ITO (at its optimal free-carrier concentration) as the material here due to its near-optimality for near-field RHT. However, this material is not necessarily optimized for a particular subwavelength patterning strategy. In fact, as shown in Fig. 10 in the main text, for deep-subwavelength patterning of periodic cylinders at 4 nm feature size, n-type InP and InAs can outperform the optimal ITO. However, even the HTC from the best effective-medium metamaterial (that from n-type InP in our investigation) is less than a factor of 2 improvement from the bulk, unpatterned optimal value provided by ITO, and smaller than the that from bulk ideal metal. Clearly, under effective material parameters, whether isotropic or anisotropic, nearly the best HTC values can be provided by simple bulk materials.

![FIG. S7: HTCs from hyperbolic metamaterials of thin stacks of materials and air, as a function of feature size for a unit cell fixed at 50 nm thickness. For ideal materials (metal, ITO, CdO at their optimal carrier concentrations), the unpatterned HTC (right-most axis) always offer better HTC levels than the thin-film patterned ones. For materials with much higher than ideal carrier concentrations (n-type InP, n-type InAs, n-type Si, Zn$_{0.982}$Ga$_{0.018}$O), patterning can provide a decent amount of improvement. Such patterning does not help polar dielectrics (SiC). Solid triangles indicate materials with experimentally measured permittivity data at the required carrier concentrations, while hollow triangles indicate the need for such measurements. All finite-feature-size data uses effective-medium theory and may overestimate HTC. Such patterning provide enhancement no where near that from in-plane patterning of 2D cylindrical holes.](image-url)
isotropically patterned 3D air-holes. Conclusions similar to those from 2D in-plane patterning of cylindrical holes can be drawn. The decrease in carrier concentration helps decrease $\epsilon_b$ and $\omega_p$, providing broader bandwidth and better alignment with $\omega_{\text{Wien}}$. The optimal feature size is the one that helps achieve the best overall effects for HTC in terms of bandwidth and resonance frequency. Under certain feature sizes, the former patterning scheme can even beat the latter. However, the latter is of more practical interesting due to fabrication considerations. Whichever the patterning scheme and whatever the feature size, the HTCs of the patterned cases do not surpass $2.6 \times 10^5 \text{W/(m}^2\text{K)}$, the upper bound provided by the causality constrained numerical optimizations.

Fig. S7 details the HTCs from hyperbolic metamaterials of thin stacks of materials and air, as a function of feature size, i.e. the material thickness. For all optimal and some of the sub-optimal materials, such patterning will not provide improvement, no matter what the feature size. Only when the bulk parameters are bad enough, for example, n-type InP, n-type InAs and n-type Si that have large $\epsilon_b$, or Zn$_{0.98}$Ga$_{0.02}$O$_{1.01}$O that have large $\omega_p$, HTC enhancement at the optimal fill fraction is decent but not as good as the other two types of patterning described above. As illustrated by the example of ITO, the mechanism of HTC enhancement is different for hyperbolic materials, as relatively narrow-band gap surface modes are now replaced by broadband hyperbolic modes. As these modes are far less well-confined to the interfaces, compromising photon exchanges across the interfaces, they are by no means ideal for heat transfer. This mechanism does not affect the resonance frequency or increase the resonance strength either, confirming again HTC levels of polar dielectrics are barely improved from nano-patterning.

Notably, all the predicted HTCs from effective-medium approximations can only hold as gap distances are adequately large, temperatures adequately low, and unit-cell sizes and feature sizes adequately small. They are likely overestimates when the gap distances are small.

VIII. OPTICAL PROPERTIES OF 2D PLASMONIC MATERIALS AND THEIR NEAR-FIELD HTCS

At the air interface of a 2D polaritonic medium with conductivity $\sigma(\omega, \beta)$ with substrate $\epsilon_{\text{sub}}$, the reflectivity is given by

$$r(\omega, \beta) = -1 + \frac{k_{\text{sub},z}}{k_{0,z}} \frac{2\epsilon_0\omega}{2\epsilon_0\epsilon_0\omega + k_{\text{sub},z}\sigma(\omega, \beta)},$$

(S33)

while the 2D surface wave dispersion is given by [5]

$$\frac{\epsilon_{\text{sub}}}{k_{\text{sub},z}} + \frac{1}{k_{0,z}} = -\frac{\sigma(\omega, \beta)}{\omega\epsilon_0},$$

(S34)

where $k_{\text{sub},z} = \sqrt{\epsilon_{\text{sub}}\omega^2 - \beta^2}$.

Following the notations from the main text, a simple 2D plasmonic conductivity with negligible spatial dispersion can be written as

$$\sigma(\omega) = i\epsilon_0\omega t \frac{\omega_b^2}{\omega^2 + i\gamma \omega}.$$  

(S35)

The 2D surface wave dispersion in the non-retarded regime is

$$\beta = \frac{2}{t} \frac{\omega^2 + i\gamma \omega}{\omega_b^2},$$

(S36)

which shows the scaling of $\omega_t$ with $\sqrt{\beta}$. More precisely, through a more rigorous quasi-static analysis, it can be established that [6]

$$\omega_t^2 = \frac{\beta t}{2} \omega_b^2.$$  

(S37)

For two parallel sheets of identical 2D material in the near-field regime with separation $d$, air as substrate, the gap surface waves have dispersion

$$\left( \frac{2}{k_0} + \frac{i\sigma}{\omega\epsilon_0} \right)^2 e^{ik_{0,z}d} - \left( \frac{i\sigma}{\omega\epsilon_0} \right)^2 e^{-ik_{0,z}d} = 0.$$  

(S38)
With the simple 2D conductivity model as Eq. (S35) and the optimal parameters, these 2D gap surface waves provide modal photon exchange as shown in Fig. S9(a), which also leads to the 2D material spectral photon exchange profile in Fig. 5 of the main text.

We also compute the HTC from $\sigma_{2D}$ of 2D materials reported in literature, such as graphene whose intraband electronic transitions dominate its optical properties in the infrared:

$$\sigma_{\text{intra}}(\omega, T) = \frac{2\epsilon_0 e^2 T}{\pi \hbar (\omega + \gamma)} \ln \left( 2 \cosh \frac{E_F}{2T} \right),$$  \hspace{1cm}  \text{(S39)}$$

where $E_F$ is the Fermi level, and $E_F = 0.4 \text{eV}$ gives to the graphene HTC in Fig. 10 of the main text.

**IX. WIEN FREQUENCIES FOR 2D PLASMONIC MATERIALS**

Although the 2D plasmons can have quite different modal dispersions from the bulk ones, they are by nature still narrow-band compared to the dispersion and density of states for propagating plane waves. Therefore, to a large degree, the Wien analysis similar to that of the optimal bulk Drude materials can apply. To be exact, we numerically identified $\omega_{\text{Wien}}$ for 2D plasmonic materials, and plot them in tandem with those of the bulk Drude ones in Fig. S8. At their optimal loss rate which is around $g = 0.06$ for the temperature range of interest, the HTC Wien frequencies of 2D materials are quite similar to those of bulk Drude materials, with a slight blue shift due to the slightly wider bandwidth of the dispersion from two sheets of 2D materials.

![Image](image_url)

**FIG. S8:** Wien frequencies of 2D and bulk plasmonic materials for the near-field planar-planar configuration. The red curve for the “bulk Drude” case can be analytically derived (Eq. (S23)), whereas the grey curve for “2D plasmonic” is numerically identified for each $T$.

**X. 2D PLASMONIC MATERIALS WITH DIFFERENT SUBSTRATE REFRACTIVE INDICES**

The 2D surface wave dispersion and therefore RHT can be quite sensitive to the substrate permittivity for 2D materials. Without much loss of generality, we assume that the substrate has negligible polaritonic response in the frequency range we are interested in, and thus can be modeled by a constant permittivity, or refractive index. As a general rule of thumb, the higher the substrate refractive index, the higher the optimal $\omega_b$ and the lower the optimal $g$. As can be seen from the comparison between Fig. S9(a) and (b), where both are using optimal parameters for their respective $\epsilon_{\text{sub}}$, a larger $\epsilon_{\text{sub}}$ leads to much narrower modal bandwidth of 2D surface waves, thus smaller spectral contribution to HTC at the resonant frequencies. More generally, more resonances and better confinement can be supported had there been larger index contrast, which makes vacuum the best substrate in theory for the 2D materials of interest here.
FIG. S9: Modal photon exchange of the optimal 2D plasmonic material at $d = 10$ nm, for (a) air substrate and (b) substrate with $\epsilon_{\text{sub}} = 4$.

XI. GAP DISTANCE DEPENDENCE OF OPTIMAL $\omega_b$ AND $n_{2D}$ FOR 2D PLASMONIC MATERIALS

We parametrically optimize $\omega_b$ and $g$ pairs for the 2D conductivity in Eq. (S35) for every gap separation $d$, and find the ones maximizing HTC. In Fig. S10 we present these optimal parameters for $d$ ranging from 10 to 1000 nm that lead to the optimal “2D plasmonic” curves in the main text. Although the scaling factor depends on the dummy-variable thickness $t$, which is assumed to be 1 nm throughout, the scaling relation of optimal $\omega_b \sim \sqrt{d}$ is general no matter what the electronic dispersion. As for the carrier concentration for materials with Dirac linear dispersion, as we shown in Fig. S10, optimal $n_{2D} = 9 \times 10^{11}$ cm$^{-2}$ $\times \left(\frac{d}{100 \text{ nm}}\right)^2$, independent of the assumed length scale $t$.

FIG. S10: Optimal $\omega_b$ (assuming dummy-variable thickness $t = 1$ nm) and $n_{2D}$ (assuming Dirac linear dispersion) for 2D plasmonic materials at different gap separations for temperature $T = 300$ K and substrate $\epsilon_{\text{sub}} = 1$.